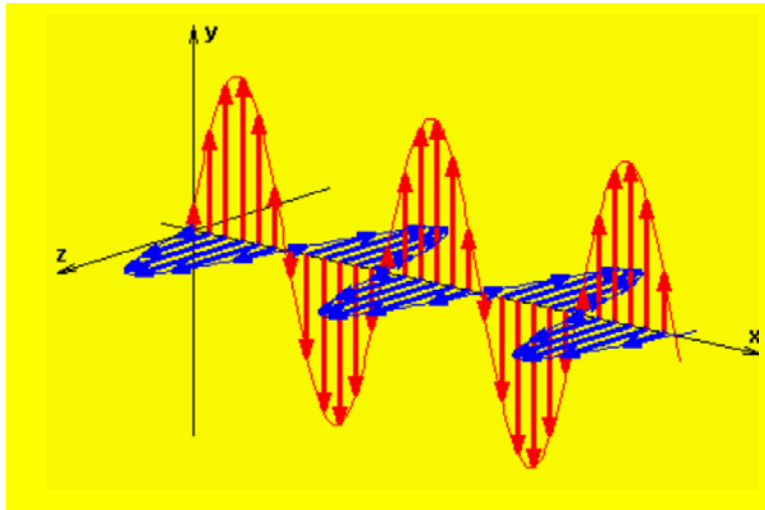


OPTI 380A

Intermediate Optics Lab 7: Waveplates and Stokes Vectors

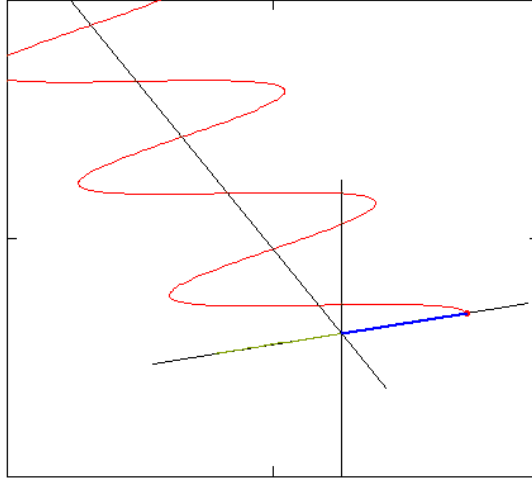
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Linearly Polarized EM Wave



Various States of Polarization

pol_{state} = "Linear polarized in x"



Simulation by Bernd Geh of Zeiss

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Polarization

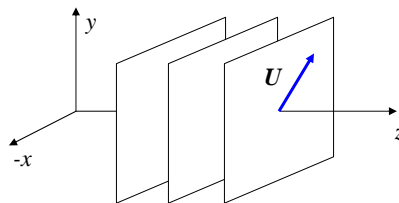
Consider the case of an EM plane wave traveling in the +z direction.

E oscillates perpendicular to z .

General solution:

$$\mathbf{U}(z, t) = U_0 e^{j(kz - \omega t)} = [A_x \hat{x} + A_y e^{j\phi} \hat{y}] e^{j(kz - \omega t)} \quad A_x, A_y \in \text{Re}\{ \}$$

We will now trace the tip of the electric vector for several special cases.



We will look at both:

fixed $z = z_0$ with $t = \text{variable}$

fixed $t = t_0$ with $z = \text{variable}$

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Polarization – Linear

$$\phi = 0$$

Special case where $A_x = A_y = A_0$:

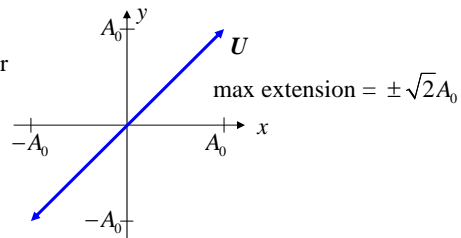
$$U(z,t) = A_0 (\hat{x} + \hat{y}) e^{j(kz - \omega t)}$$

$$\text{Re}[U(z,t)] = A_0 (\hat{x} + \hat{y}) \cos(kz - \omega t) \leftarrow \text{This is the physical wave.}$$

Consider $z = z_0$, where $\text{Re}[U(z_0,t)] = A_0 (\hat{x} + \hat{y}) \cos(kz_0 - \omega t)$

Trace the tip of the electric vector in the (x,y) plane in time:

This is true for all z_0 .



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Polarization – Left Circular

$$A_x = A_y = A_0$$

$$\phi = \pi/2$$

$$U(z,t) = A_0 [\hat{x} + e^{j\pi/2} \hat{y}] e^{j(kz - \omega t)}$$

Consider $z = 0$, where

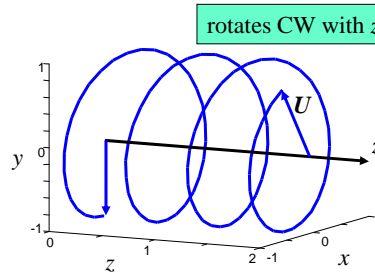
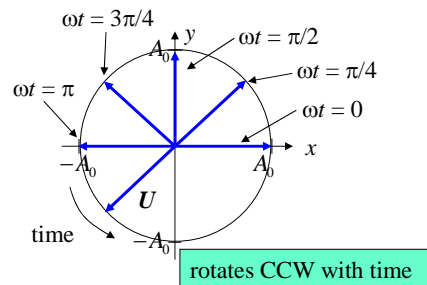
$$\text{Re}\{U(0,t)\} = A_0 [\cos(\omega t)\hat{x} + \cos(\pi/2 - \omega t)\hat{y}]$$

$$= A_0 [\cos(\omega t)\hat{x} + \sin(\omega t)\hat{y}]$$

Consider $t = 0$, where

$$\text{Re}\{U(z,0)\} = A_0 [\cos(kz)\hat{x} + \cos(\pi/2 + kz)\hat{y}]$$

$$= A_0 [\cos(kz)\hat{x} - \sin(kz)\hat{y}]$$



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Polarization – Right Circular

$$A_x = A_y = A_0$$

$$\phi = -\pi/2$$

$$U(z, t) = A_0 [\hat{x} + e^{-j\pi/2} \hat{y}] e^{j(kz - \omega t)}$$

Consider $z = 0$, where

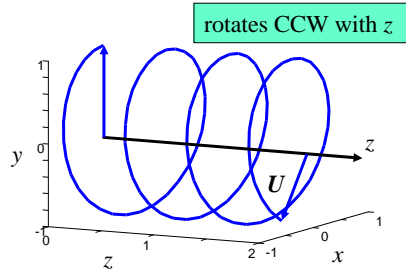
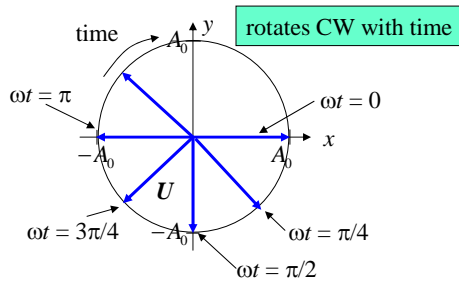
Consider $t = 0$, where

$$\text{Re}\{U(0, t)\} = A_0 [\cos(\omega t) \hat{x} + \cos(-\pi/2 - \omega t) \hat{y}]$$

$$\text{Re}\{U(z, 0)\} = A_0 [\cos(kz) \hat{x} + \cos(-\pi/2 + kz) \hat{y}]$$

$$= A_0 [\cos(\omega t) \hat{x} - \sin(\omega t) \hat{y}]$$

$$= A_0 [\cos(kz) \hat{x} + \sin(kz) \hat{y}]$$



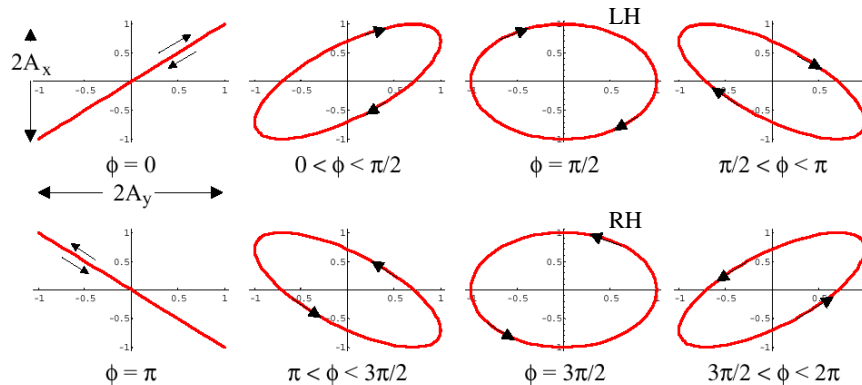
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Polarization – Elliptical

(Arrows show trace in z direction)



This slide from Jim Wyant, 2000.

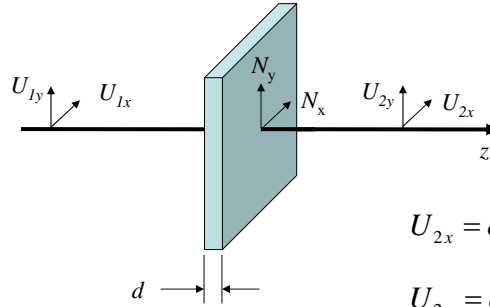
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Polarization – Waveplates

Consider optical elements with polarization-dependent refractive index.



$$N_x = n_x + j\kappa_x$$

$$N_y = n_y + j\kappa_y$$

$$U_{2x} = e^{j\frac{2\pi}{\lambda}n_x d} e^{-\frac{2\pi}{\lambda}\kappa_x d} U_{1x}$$

$$U_{2y} = e^{j\frac{2\pi}{\lambda}n_y d} e^{-\frac{2\pi}{\lambda}\kappa_y d} U_{1y}$$

Retardation plate: $n_x \neq n_y, \kappa_x \approx \kappa_y \approx 0$
Polarizer plate: $n_x \approx n_y, \kappa_x \neq \kappa_y$

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Half-Wave Retardation Plate

The thickness d is fabricated so that the phase difference between x and y polarization components through the plate is π .

$$U_{2x} \approx e^{j\frac{2\pi}{\lambda}n_x d} U_{1x}$$

$$U_{2y} \approx e^{j\frac{2\pi}{\lambda}n_y d} U_{1y}$$

Change in
phase through
the plate:

$$\Delta\phi_{2x} = \frac{2\pi}{\lambda} n_x d$$

$$\Delta\phi_{2y} = \frac{2\pi}{\lambda} n_y d$$

Note that one axis introduces more phase than the other, because the wave velocity is slower. Therefore, it is called the "slow" axis. The other axis is the "fast" axis.

$$\Delta\phi_{2x} - \Delta\phi_{2y} = \frac{2\pi}{\lambda} (n_x - n_y) d = \pi$$

Solving for d :

$$d = \frac{\lambda}{2|n_x - n_y|}$$

Usually, crystal axes are called "ordinary" n_o and "extraordinary" n_e instead of n_x and n_y .

Example: Quartz
 $n_o = n_x = 1.544$
 $n_e = n_y = 1.553$
at $\lambda = 500$ nm

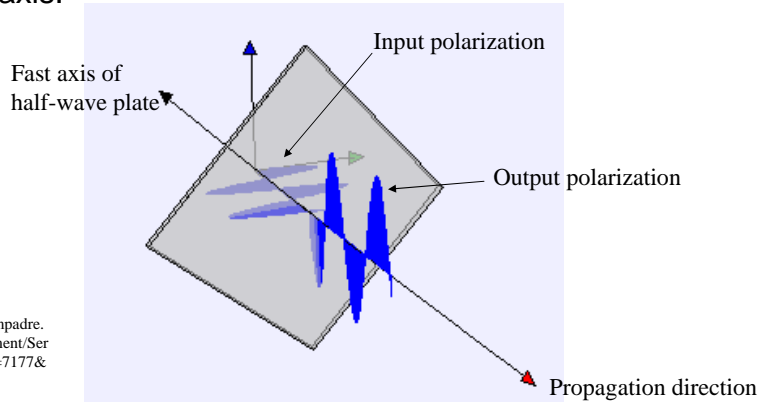
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Rotated Half-Wave Plate

- A half-wave plate rotates the output state of polarization by twice the angle between the input polarization and the fast axis.



(From <http://www.compadre.org/OSP/document/ServeFile.cfm?ID=7177&DocID=361>)

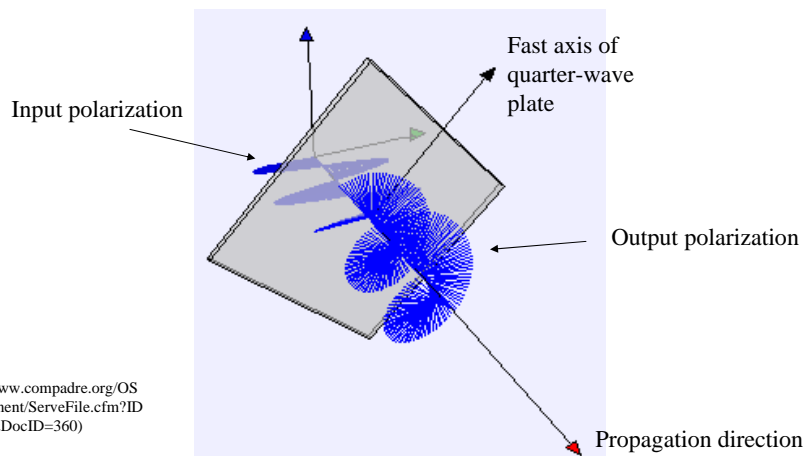
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Quarter-Wave Plate at 45°

- A quarter-wave plate rotated at 45° changes linear polarization to circular polarization.



(From <http://www.compadre.org/OSP/document/ServeFile.cfm?ID=7176&DocID=360>)

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Stokes Vectors (I)

- The preceding analysis is good for laser beams, where there is an exact relationship defining the electric field vector in time.
- Real light sources (like light bulbs and LEDs) do not emit such nicely defined light waves.
- However, transmission through polarizers, waveplates and reflections from surfaces can partially polarize the light.
- The Stokes vector is a way to describe the state of polarization for light other than laser beams.

Stokes Vectors (II)

- The four Stokes elements are:
 - S_0 is proportional to the amount of light in the beam being measured.
 - S_1 is proportional to the tendency of the light to be linearly horizontally (+) or vertically (-) polarized.
 - S_2 is proportional to the tendency of the light to be linearly $+45^\circ$ (+) or -45° (-) polarized.
 - S_3 is proportional to the tendency of the light to be RHC (+) or LHC (-).

Stokes Vectors (III)

- We determine the Stokes vector by measuring power in the beam and using a series of three filters:
 - I_0 is measurement of the beam power.
 - I_1 is measurement of power transmitted through a horizontal linear polarizer.
 - I_2 is measurement of power transmitted through a linear polarizer oriented at $+45^\circ$
 - I_3 is measurement of power transmitted through a polarizer opaque to LHC.

Stokes Vectors (IV)

- The Stokes vector is calculated from:
 - $S_0 = I_0$
 - $S_1 = 2 \cdot I_1 - I_0$
 - $S_2 = 2 \cdot I_2 - I_0$
 - $S_3 = 2 \cdot I_3 - I_0$